# Solution of time-harmonic Galbrun's equations in the context of helioseismology.

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Galbrun's equations

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Time-harmonic Galbrun's equations (pulsation  $\omega$ )

$$\begin{cases} -\rho_0 \left( -i\omega + \sigma + M \cdot \nabla \right)^2 \boldsymbol{u} - \nabla \left( \rho_0 \, c_0^2 \operatorname{div} \boldsymbol{u} \right) \\ + (\operatorname{div} \boldsymbol{u}) \, \nabla \rho_0 - (\nabla \boldsymbol{u})^T \nabla \rho_0 = f, \quad \text{in } \Omega \end{cases}$$

*u*: Lagrangian fluid displacement (unknown)

 $\rho_0$ ,  $p_0$ ,  $c_0$ : background density, pressure and sound speed  $M, \sigma$ : flow velocity and damping.

$$(\nabla \boldsymbol{u})^{\mathsf{T}} = \begin{pmatrix} \partial_{\boldsymbol{x}} \boldsymbol{u}_{\boldsymbol{x}} & \partial_{\boldsymbol{x}} \boldsymbol{u}_{\boldsymbol{y}} \\ \partial_{\boldsymbol{y}} \boldsymbol{u}_{\boldsymbol{x}} & \partial_{\boldsymbol{y}} \boldsymbol{u}_{\boldsymbol{y}} \end{pmatrix}$$

# Model problem

Time-harmonic Galbrun's equations (pulsation  $\omega$ )

$$\begin{cases} -\rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{u} - \nabla \left(\rho_0 c_0^2 \operatorname{div} \boldsymbol{u}\right) \\ + (\operatorname{div} \boldsymbol{u}) \nabla \rho_0 - (\nabla \boldsymbol{u})^T \nabla \rho_0 = \boldsymbol{f}, \quad \text{in } \Omega \end{cases}$$

*u*: Lagrangian fluid displacement (unknown)

 $\rho_0, \rho_0, c_0$ : background density, pressure and sound speed  $M, \sigma$ : flow velocity and damping.

Assumptions:

- Coefficients ρ<sub>0</sub>, p<sub>0</sub>, c<sub>0</sub>, σ, M smooth functions of x (at least continuous).
- The flow satisfies the condition  $div(\rho_0 M) = 0$

Linear equation:

 $A(x) \boldsymbol{u}(x) - \text{Div} \left[C(x) \nabla \boldsymbol{u}(x) + B(x) \boldsymbol{u}(x)\right] + E(x) \nabla \boldsymbol{u}(x) = f(x)$ where A(x), C(x), B(x), E(x) are tensors.

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# **Discontinuous Galerkin Method**

Discontinuous Galerkin formulation

$$\sum_{\kappa \text{ element}} \left( \int_{\kappa} A \, \boldsymbol{u} \cdot \varphi + (C \, \nabla \boldsymbol{u} + B \, \boldsymbol{u}) \cdot \nabla \varphi + E \, \nabla \boldsymbol{u} \cdot \varphi \, dx \right)$$

+ 
$$\sum_{F \text{ face}} \left( \int_{F} \{ C \nabla \boldsymbol{u} \nu \} [\varphi] + [\boldsymbol{u}] \{ C \nabla \varphi \nu \} + \{ B \boldsymbol{u} \nu \} [\varphi] + [\boldsymbol{u}] \{ E^* \varphi \nu \} \right)$$

$$+\frac{1}{2}[P u][\varphi] dx + \int_{\Gamma} N u \cdot \varphi dx = \sum_{\kappa \text{ element}} \int_{\kappa} f \cdot \varphi dx$$

where

$$\{u\} = \frac{u^+ + u^-}{2}, \quad [u] = (u^+ - u^-)$$

 $\nu$  : outward normale

P, N : penalty matrix and boundary condition matrix

Discontinuous Galerkin applied directly  $\Rightarrow$  SIPG

$$\begin{cases} -\rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{u} - \nabla \left(\rho_0 c_0^2 \operatorname{div} \boldsymbol{u}\right) \\ + (\operatorname{div} \boldsymbol{u}) \nabla p_0 - (\nabla \boldsymbol{u})^T \nabla p_0 = \boldsymbol{f}, & \text{in } \Omega \end{cases}$$

Penalty matrix:

$$\boldsymbol{P} = \alpha \frac{r(r+1)}{h^2} \nu \nu^T$$

*r*: order of approximation *h*: length of the edge In practice, we took  $\alpha = 10$  and observed numerically a positive stiffness matrix for a null flow.

Equivalent first-order formulation:

$$\begin{cases} \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \boldsymbol{u} - \rho_0 \boldsymbol{v} = \boldsymbol{0} \\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \boldsymbol{v} - \nabla(\rho_0 c_0^2 \boldsymbol{p}) + (\operatorname{div} \boldsymbol{u}) \nabla p_0 - (\nabla \boldsymbol{u})^T \nabla p_0 = \boldsymbol{f} \\ \boldsymbol{p} - \operatorname{div} \boldsymbol{u} = \boldsymbol{0} \end{cases}$$

- Upwind fluxes difficult to implement
- Not adapted for explicit time-stepping

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Better equivalent first-order formulation  $\Rightarrow$  LDG

$$\rho_{0} (-i\omega + \sigma + M \cdot \nabla) \boldsymbol{u} - \nabla \boldsymbol{p} - \rho_{0} \boldsymbol{q} = \boldsymbol{0}$$

$$\rho_{0} (-i\omega + \sigma + M \cdot \nabla) \boldsymbol{q} - (\nabla \sigma) \boldsymbol{p} - (\nabla M)^{T} \nabla \boldsymbol{p} - \frac{M \cdot \nabla \rho_{0}}{\rho_{0}} \nabla \boldsymbol{p}$$

$$+ (\operatorname{div} \boldsymbol{u}) \nabla \rho_{0} - (\nabla \boldsymbol{u})^{T} \nabla \rho_{0} = \boldsymbol{f}$$

$$\rho_{0} (-i\omega + \sigma + M \cdot \nabla) \boldsymbol{p} - \rho_{0}^{2} c_{0}^{2} \operatorname{div} \boldsymbol{u} = \boldsymbol{0}$$

- Well adapted for explicit time-stepping
- Form close to an hyperbolic system

#### Considered equation

$$A(x) \mathbf{u}(x) - \mathsf{Div} \left[B(x) \mathbf{u}(x)\right] + E(x) \nabla \mathbf{u}(x) = f(x)$$

Matrix D(x) defined as:

$$D(x) = -B(x)\nu + E(x)\nu$$

A(x) decomposed as

$$A(x) = -i\omega M(x) + A_0(x)$$

A, V eigenvalues and eigenvectors of  $M(x)^{-1}D(x)$ 

#### $\Lambda$ , V eigenvalues and eigenvectors of $M^{-1}D$

 $M^{-1}D = V \wedge V^{-1}$ 

Absolute value of *D* defined as:

 $|D| = M V |\Lambda| V^{-1}$ 

Upwind fluxes  $\Rightarrow$  penalty matrix *P*:

P = |D|

Eigenvalues A real if the system is hyperbolic

A (1) > A (1) > A

#### Uniform flow:

$$\boldsymbol{M} = \rho_0 \boldsymbol{I}, \quad \boldsymbol{D} = \begin{pmatrix} \rho_0 \alpha & 0 & 0 & 0 & -\nu_{\boldsymbol{X}} \\ 0 & \rho_0 \alpha & 0 & 0 & -\nu_{\boldsymbol{Y}} \\ 0 & 0 & \rho_0 \alpha & 0 & 0 \\ 0 & 0 & 0 & \rho_0 \alpha & 0 \\ -(\rho_0 c_0)^2 \nu_{\boldsymbol{X}} & -(\rho_0 c_0)^2 \nu_{\boldsymbol{Y}} & 0 & 0 & \rho_0 \alpha \end{pmatrix}$$

where

 $\alpha = M \cdot \nu$ 

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Uniform flow :

$$\Lambda = \begin{pmatrix} \alpha \\ \alpha \\ \alpha \\ \alpha + c_0 \\ \alpha - c_0 \end{pmatrix}, \ |D| = \rho_0 \begin{pmatrix} |\alpha| \mathbb{I} + (s - |\alpha|) \nu \nu^T & 0 & -\frac{d}{\rho_0 c_0} \nu \\ 0 & |\alpha| \mathbb{I} & 0 \\ -\rho_0 c_0 d\nu^T & 0 & s \end{pmatrix}$$

where

$$s = rac{1}{2} \left( |lpha + c_0| + |lpha - c_0| 
ight), \quad d = rac{1}{2} \left( |lpha + c_0| - |lpha - c_0| 
ight)$$

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Non-uniform flow :

$$\boldsymbol{M} = \rho_0 \boldsymbol{I}, \quad \boldsymbol{D} = \begin{pmatrix} \rho_0 \alpha & 0 & 0 & 0 & -\nu_{\boldsymbol{X}} \\ 0 & \rho_0 \alpha & 0 & 0 & -\nu_{\boldsymbol{Y}} \\ 0 & \rho_0 \gamma & \rho_0 \alpha & 0 & \beta_{\boldsymbol{X}} \\ -\rho_0 \gamma & 0 & 0 & \rho_0 \alpha & \beta_{\boldsymbol{Y}} \\ -(\rho_0 c_0)^2 \nu_{\boldsymbol{X}} & -(\rho_0 c_0)^2 \nu_{\boldsymbol{Y}} & 0 & 0 & \rho_0 \alpha \end{pmatrix}$$

where

$$\boldsymbol{\alpha} = \boldsymbol{M} \cdot \boldsymbol{\nu}, \quad \rho_0 \boldsymbol{\gamma} = \nabla \boldsymbol{p}_0 \times \boldsymbol{\nu}$$
$$(\beta_{\boldsymbol{X}}, \beta_{\boldsymbol{Y}}) = (-\nabla \boldsymbol{M})^T \boldsymbol{\nu} - \frac{\boldsymbol{M} \cdot \nabla \rho_0}{\rho_0} \boldsymbol{\nu}$$

Issue : D is not diagonalizable if  $\gamma, \beta_x, \beta_y \neq 0$ 

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#### Non-uniform flow :

$$\boldsymbol{M} = \rho_0 \boldsymbol{I}, \quad \boldsymbol{D} = \begin{pmatrix} \rho_0 \alpha & 0 & 0 & 0 & -\nu_x \\ 0 & \rho_0 \alpha & 0 & 0 & -\nu_y \\ 0 & \rho_0 \gamma & \rho_0 \alpha_1 & 0 & \beta_x \\ -\rho_0 \gamma & 0 & 0 & \rho_0 \alpha_1 & \beta_y \\ -(\rho_0 c_0)^2 \nu_x & -(\rho_0 c_0)^2 \nu_y & 0 & 0 & \rho_0 \alpha \end{pmatrix}$$

*D* diagonalizable if  $\alpha_1 \notin \{\alpha, \alpha + c_0, \alpha - c_0\}$ Penalty matrix:

$$P = \lim_{\alpha_1 \to \alpha} |D|_{\alpha_1}$$

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# $H^1$ formulation

Formulation proposed by Bonnet Ben Dhia et al (in 2-D):

$$\begin{cases} \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{u} - \nabla \left(\rho_0 c_0^2 \operatorname{div} \boldsymbol{u}\right) + \operatorname{curl}\left(\rho_0 c_0^2 \left(\operatorname{curl}(\boldsymbol{u}) - \boldsymbol{\psi}\right)\right) \\ + \left(\operatorname{div} \boldsymbol{u}\right) \nabla \rho_0 - \left(\nabla \boldsymbol{u}\right)^T \nabla \rho_0 = f \\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{\psi} + 2\rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \mathcal{B}(\boldsymbol{u}) + \rho_0 \mathcal{C}(\boldsymbol{u}) \\ = -\operatorname{curl}(f) + \frac{1}{\rho_0 c_0^2} f \wedge \nabla \rho_0 \end{cases}$$

$$\mathcal{B}(\boldsymbol{u}) = \sum_{j=1}^{2} \nabla M_{j} \wedge \frac{\partial \boldsymbol{u}}{\partial x_{j}}$$

$$\begin{aligned} \mathcal{C}(\boldsymbol{u}) &= \sum_{j,k=1}^{2} \left( \frac{\partial M_{k}}{\partial x_{j}} \nabla M_{j} \wedge \frac{\partial \boldsymbol{u}}{\partial x_{k}} - M_{j} \nabla \frac{\partial M_{k}}{\partial x_{j}} \wedge \frac{\partial \boldsymbol{u}}{\partial x_{k}} \right) \\ &+ \frac{1}{\rho_{0}} \sum_{j=1}^{2} \left( \frac{1}{\rho_{0} c_{0}^{2}} \frac{\partial \rho_{0}}{\partial x_{j}} \nabla p_{0} - \nabla \left( \frac{\partial \rho_{0}}{\partial x_{j}} \right) \right) \wedge \nabla \boldsymbol{u}_{j} \end{aligned}$$

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Formulation proposed by Bonnet Ben Dhia et al (in 2-D):

$$\begin{cases} \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{u} - \nabla \left(\rho_0 c_0^2 \operatorname{div} \boldsymbol{u}\right) + \operatorname{curl}\left(\rho_0 c_0^2 \left(\operatorname{curl}(\boldsymbol{u}) - \boldsymbol{\psi}\right)\right) \\ + (\operatorname{div} \boldsymbol{u}) \nabla \rho_0 - (\nabla \boldsymbol{u})^T \nabla \rho_0 = f \\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right)^2 \boldsymbol{\psi} + 2\rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \mathcal{B}(\boldsymbol{u}) + \rho_0 \mathcal{C}(\boldsymbol{u}) \\ = -\operatorname{curl}(f) + \frac{1}{\rho_0 c_0^2} f \wedge \nabla \rho_0 \end{cases}$$

- Continuous finite elements for  $u, \psi \Rightarrow H^1$
- Discontinuous finite elements for  $\boldsymbol{u}, \boldsymbol{\psi} \Rightarrow \mathbf{H}^{1}(\mathbf{DG})$

Uniform coefficients:

$$M = (m_x, 0), \ \rho_0 = 2.5, \ c_0 = 0.8, \ \rho_0 = 1, \ \omega = 0.78 \times 2 \pi, \ \sigma = 0.1$$

Computational domain:

$$\Omega = [-4, 4]^2$$

Gaussian source:

$$f = \beta_0 \exp(-\alpha_0(x^2 + y^2))e_x$$

Periodic boundary conditions *h*: mesh size, *r*: degree of polynomial space

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## Results for an uniform flow



Figure: Real part of  $u_x$  (left) and  $u_y$  (right) for an uniform flow  $m_x = 0.25$ 

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### Results for an uniform flow



Figure: Real part of  $u_x$  (left) and  $u_y$  (right) for an uniform flow  $m_x = 0.75$ 

## Results for an uniform flow



Figure: Real part of  $u_x$  (left) and  $u_y$  (right) for an uniform flow  $m_x = 1.5$ 



Figure: Relative  $L^2$  error vs h/r for LDG quadrilateral elements and an uniform flow ( $m_x = 0.25$ ).



Figure: Comparison of the different formulations for an uniform flow ( $r = 5, m_x = 0.25$ )



Figure: Convergence observed for any value  $m_x$ .

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Physical coefficients are chosen periodic :

$$\rho_{0} = 1.5 + 0.2 \cos\left(\frac{\pi x}{4}\right) \sin\left(\frac{\pi y}{2}\right)$$

$$p_{0} = 1.44\rho_{0} + 0.08\rho_{0}^{2}$$

$$c_{0}^{2} = 1.44 + 0.16\rho_{0}$$

$$\omega = 0.78 \times 2\pi, \quad \sigma = 0.1$$

The flow *M* satisfies  $div(\rho_0 M) = 0$ :

$$m_x = \operatorname{coeff}\left(\frac{0.3 + 0.1\cos\left(\frac{\pi y}{4}\right)}{\rho_0}\right)$$
$$m_y = \operatorname{coeff}\left(\frac{0.2 + 0.08\sin\left(\frac{\pi x}{4}\right)}{\rho_0}\right)$$



Figure: Numerical solution obtained with  $H^1$  formulation, with N = 61 points (left) and N = 81 points (right) and r = 10, coeff = 0.1.



Figure: Numerical solution obtained with  $H^1$  formulation with N = 41 points (left) and N = 61 points (right) and r = 10, coeff = 0.2



Figure: Numerical solution obtained with  $H^1$  formulation with N = 41 points (left) and N = 61 points (right) and r = 10, coeff = 1.5

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Figure: Convergence for non-uniform flow coeff =  $0.1, r = 5, ||M||_{\infty} \approx 0.033$ .



Figure: Convergence for non-uniform flow coeff =  $0.2, r = 5, ||M||_{\infty} \approx 0.067.$ 



Figure: Convergence for non-uniform flow coeff = 0.5, r = 5,  $||M||_{\infty} \approx 0.15$ ,



Figure: Convergence for non-uniform flow coeff =  $1.5, r = 5, ||M||_{\infty} \approx 0.5, ..., 0.5$ 



Figure: Consistency error for LDG formulation (r = 10), upwind fluxes.



Figure: Consistency error for  $H^1$  formulation (r = 10).

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$$\begin{cases} (-i\omega + \sigma + M \cdot \nabla)p + \operatorname{div}(c_0^2 u) + \gamma(\operatorname{div} M)p - \frac{(\gamma - 1)}{\rho_0}u \cdot \nabla p_0 = 0\\ (-i\omega + \sigma + M \cdot \nabla)\rho + \rho \operatorname{div} M + \operatorname{div} u = 0\\ (-i\omega + \sigma + M \cdot \nabla)u + (\operatorname{div} M)u + \nabla p + \nabla M(u + \rho M) = \frac{g}{\rho_0}\\ \rho, p, u \text{ perburbations } (\rho', \rho_0 u', p')\\ \gamma \text{ defined by } c_0^2 = \frac{\gamma p_0}{\rho_0} \end{cases}$$

Equivalence with Galbrun's equations for uniform flow if:

$$f = (-i\omega + \sigma + M \cdot \nabla)g$$



Figure: Solution obtained with Galbrun's equation (left) and LEE (right) (coeff = 0.1, real part of  $u_x$ ).



Figure: Solution obtained with Galbrun's equation (left) and LEE (right) (coeff = 0.2, real part of  $u_x$ ).



Figure: Solution obtained with Galbrun's equation (left) and LEE (right) (coeff = 0.5, real part of  $u_x$ ).



Figure: Comparison for coeff=1.5.

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#### Convergence for LEE



#### Figure: Convergence for non-uniform flow and LEE (r = 10).

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Convective stabilization :

$$\begin{cases} \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) u - \nabla p - \rho_0 q = 0\\ \rho_0 \left(-i\omega + \sigma\right) q - (\nabla \sigma) p - (\nabla M)^T \nabla p - \frac{M \cdot \nabla \rho_0}{\rho_0} \nabla p \\ + (\operatorname{div} u) \nabla \rho_0 - (\nabla u)^T \nabla \rho_0 = f\\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) p - \rho_0^2 c_0^2 \operatorname{div} u = 0 \end{cases}$$

Non-uniform stabilization:

$$\begin{cases} \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \boldsymbol{u} - \nabla \boldsymbol{p} - \rho_0 \, \boldsymbol{q} = \boldsymbol{0} \\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \boldsymbol{q} = \boldsymbol{f} \\ \rho_0 \left(-i\omega + \sigma + M \cdot \nabla\right) \boldsymbol{p} - \rho_0^2 \, c_0^2 \operatorname{div} \boldsymbol{u} = \boldsymbol{0} \end{cases}$$

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## Stabilization of Galbrun's equations



Figure: Real part of  $u_x$  for a non-uniform flow (coeff=1.5) and stabilized Galbrun's equations (on left, convective stabilization, on right non-uniform stabilization)

Equivalent to Galbrun's equations when M = 0

$$\begin{cases} \rho_0(-i\omega + \sigma + M \cdot \nabla) \mathbf{p} + \rho_0^2 c_0^2 \operatorname{div} \mathbf{u} = \mathbf{0} \\ \rho_0(-i\omega + \sigma + M \cdot \nabla) \mathbf{u} + \nabla \mathbf{p} \\ + \frac{1}{-i\omega + \sigma} \left( (\operatorname{div} \mathbf{u}) \nabla p_0 - (\nabla \mathbf{u})^T \nabla p_0 \right) = \mathbf{g} \end{cases}$$

# Simplified Galbrun's equations



Figure: Convergence for non-uniform flow and simplified Galbrun  $(r = 10)_{10}$ 

#### Computation of Green's function

$$g = \delta e_y, M = (0, 0.3)$$



#### Figure: Imaginary part of $u_y$ and associated mesh.

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#### Computation of Green's function

$$g = \delta e_y, M = (0, 0.3)$$



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### Computation of Green's function

#### Non-uniform flow and mesh only refined at the center



#### Figure: Imaginary part of $u_x$ for non-uniform flow

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#### Profile of the sound speed $c_0$ for the sun in log-scale:



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#### Profile of the backgroound density $\rho_0$ for the sun in log-scale:



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#### Profile of the background pressure $p_0$ for the sun in log-scale:



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#### Example of mesh used for 2-D experiments



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Source g gaussian centered around (0.5, 0.5) and f given as:

$$f = (-i\omega + \sigma + M \cdot \nabla)g$$

Rotating flow:

$$M = \frac{\operatorname{Coeff}}{R} c_0(r) \left[ \begin{array}{c} -y \\ x \end{array} \right]$$

Uniform damping:

$$\sigma = \frac{\omega}{100}$$

Frequency:

freq = 
$$3mHz$$
,  $\omega = 2\pi \times freq$ 

#### Numerical results for the sun



Figure: Real part of  $u_x$  for the sun (Coeff = 0, Galbrun).

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#### Numerical results for the sun



Figure: Real part of  $u_x$  for the sun (Coeff = 1, Galbrun).

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#### Numerical results for the sun



Figure: Real part of  $u_x$  for the sun (Coeff = 1, simplified Galbrun).

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