



High order numerical methods for moments models

Katia Ait Ameur (CMAP, École Polytechnique)

M. Essadki, S. Kokh, M. Massot, T. Pichard,

23-11-2022

Outline

1 Context

- Global
- Transport of a polydisperse spray

2 Realizable high order methods

- Kinetic Finite Volume schemes
- Runge Kutta Discontinuous Galerkin methods

3 Slope limitation

- Principle
- Properties
- Projection method

4 Numerical results

Outline

1 Context

- Global
- Transport of a polydisperse spray

2 Realizable high order methods

- Kinetic Finite Volume schemes
- Runge Kutta Discontinuous Galerkin methods

3 Slope limitation

- Principle
- Properties
- Projection method

4 Numerical results

Two-phase flows in combustion engines



Source: C. Dumouchel CORIA Rouen

Industrial applications

Liquid propulsion: aeronautic or automotive combustion chambers

- Combustion of polydisperse evaporating sprays
- Soots formation

Global objective: Predict, using simulations, the dynamic and evaporation of the spray stemming from the atomization of the liquid phase.

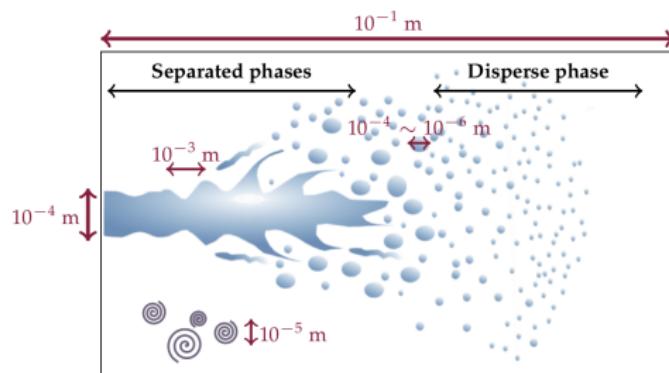
Multi-scales two-phase flow: separated and disperse phases

Separated phases

DNS, Front tracking (Glimm et al, 2001), Interface capturing: Level Set (Osher, Sethian, 1988))

Disperse phases

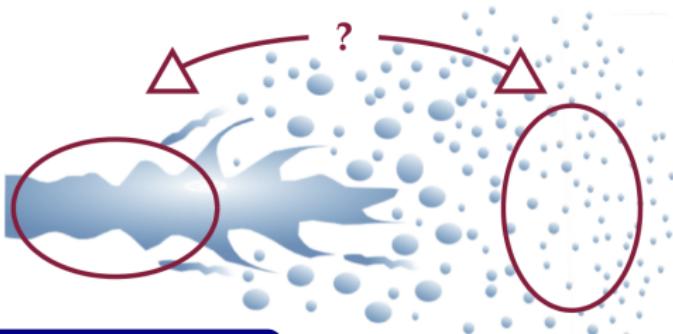
Kinetic model: Population Balance equation (Williams, 1958)



Reduced-order models

- Computational cost: $N_{cells} > 10^9$, $N_{iter} > 10^6$
- Averaged two-fluid models (Baer, Nunziato, 1986): modeling sub-scale interface
- Eulerian moment method

Coupling strategies



Litterature review

- (Vallet et al, 2001), averaged two-fluid model + Lagrangian model
- (Herrmann, 2013), interface capturing method + Lagrangian approach
- (Le Touze, 2015), two-fluid model + kinetic based moment model
- (Drui, 2017), (Cordesse,2020), (Loison, 2023), averaged model enriched with small scales dynamics

Our strategy

- Use a unified set of variables to describe the interface topology
- Enriched averaged two-phase flows with geometrical variables
- **Moment models to describe the disperse phase (Essadki, 2020)**

Modeling of the disperse phase

Internal variables ξ : droplet size S , velocity c :

$$f(x, \xi, t) \quad \Omega = \mathbb{R}_+ \times \mathbb{R}^d \times \mathbb{R}_+$$

Population Balance Equation, Williams Boltzmann equation: (Williams, 1958)

$$\partial_t f + \partial_x(c f) = 0$$

Moments:

$$m_k(t, x) = \int_{\Omega} \xi^k f(x, \xi, t) d\xi$$

Equations for a finite number of moments:

$$\partial_t m_k + \partial_x \left(\int_{\Omega} \xi^k c f d\xi \right) = 0$$

Issues

- The equations needs to be closed
- Reconstruction of the NDF from the moments
- Design realizable numerical schemes

Kinetic modeling of the disperse phase

Number density function: $f(t, x, c, S)$

Williams-Boltzmann equation [Williams, F., 1958]:

$$\partial_t f + \partial_x(c f) = 0$$

Monokinetic closure law:

$$f(t, x, c, S) = n(t, x, S) \delta(c - u).$$

Eulerian moment method

- Velocity moments:

$$\mathcal{M}_m = \int c^m f(t, x, c, S) dc, \quad \binom{n}{nu}$$

Semi-kinetic equation:

$$\begin{cases} \partial_t n &+ \partial_x(nu) = 0, \\ \partial_t(nu) &+ \partial_x(nu^2) = 0 \end{cases}$$

- Fractionnal size moments:

$$m_{k/2} = \int S^{k/2} n(t, x, S) dS, \quad \binom{m_0}{m_{1/2}} \binom{m_1}{m_{3/2}}$$

Fractionnal high order moment model

$$\left\{ \begin{array}{lcl} \partial_t m_0 + \partial_x(m_0 u) & = & 0 \\ \partial_t m_{1/2} + \partial_x(m_{1/2} u) & = & 0 \\ \color{blue}{\partial_t m_1 + \partial_x(m_1 u)} & = & 0 \\ \partial_t m_{3/2} + \partial_x(m_{3/2} u) & = & 0 \\ \color{blue}{\partial_t(m_1 u) + \partial_x(m_1 u^2)} & = & 0 \end{array} \right.$$

Link with separated phases two-phase flow: Baer-Nunziato type models enriched with geometrical variables of the interface, [Essadki, 2018]:

- $m_{3/2}$: volume fraction
- m_1 : interfacial area density
- m_0 : average Gauss curvature
- $m_{1/2}$: mean curvature

Other strategy based on perturbation analysis of non spherical droplets [Loison et al, in preparation].

Numerical challenges

$$\begin{cases} \partial_t m_1 + \partial_x(m_1 u) = 0, \\ \partial_t(m_1 u) + \partial_x(m_1 u^2) = 0, \\ \partial_t \vec{M} + \partial_x(\vec{M} u) = 0, \quad \vec{M} = (m_0, m_{1/2}, m_{3/2}) \end{cases}$$

- **Realizability** condition:

$$\forall(t, x), \quad (m_0, m_{1/2}, m_1, m_{3/2}) \in \mathbb{M}_3^{1/2}$$

- **Maximum principle** on the velocity u
- Weakly hyperbolic, δ -shocks singularities.
- **Kinetic Finite Volume** schemes [Bouchut et al, 2003],[de Chaisemartin, 2009], [Kah et al, 2012]
- **MUSCL-Hancock** schemes [Vié, Laurent, Massot, 2013]
- **Runge Kutta Discontinuous Galerkin** schemes [Cockburn, Shu, 1989],[Zhang, Shu, 2012], [Larat et al, 2012], [Sabat, 2016]

Outline

1 Context

- Global
- Transport of a polydisperse spray

2 Realizable high order methods

- Kinetic Finite Volume schemes
- Runge Kutta Discontinuous Galerkin methods

3 Slope limitation

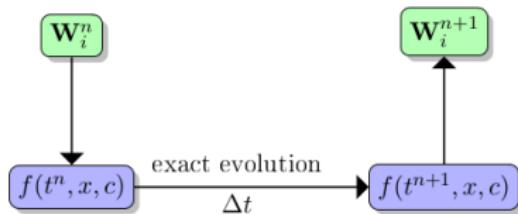
- Principle
- Properties
- Projection method

4 Numerical results

Kinetic Finite Volume scheme

$$\partial_t f + c \partial_x f = 0 \iff \begin{cases} \partial_t \rho &+ \partial_x (\rho u) = 0 \\ \partial_t (\rho u) &+ \partial_x (\rho u^2) = 0 \end{cases}$$

Exact solution: $f(t, x, c) = f(t_n, x - c(t - t_n), c)$.



Second order scheme Piecewise linear reconstruction:

$$\begin{cases} \rho(x) &= \rho_i^n + D_{\rho_i}(x - x_i), \\ u(x) &= \bar{u}_i^n + D_{u_i}(x - x_i) \end{cases}$$

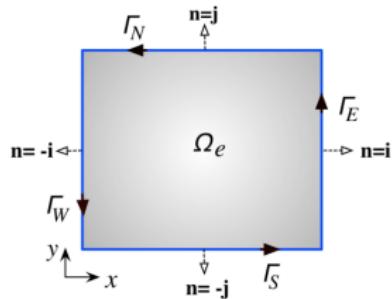
Minmod limiter [van Leer, 1974],[Toro, 2009]: realizability and stability.

DG discretization¹

$$\partial_t W + \nabla \cdot F(W) = 0$$

(k+1)-th order method: ϕ_i , basis functions of polynomials of order k .

$$W_h(x, t) = \sum_{i=0}^m W_i(t) \phi_i(x)$$



From the variational formulation:

$$\int_{\Omega_e} \partial_t W_h \phi_h d\Omega - \int_{\Omega_e} F(W_h) \cdot \nabla \phi_h d\Omega + \int_{\Gamma_e} \hat{F} \cdot n \phi_h d\Gamma = 0$$

$$M_i \frac{d\hat{W}_i}{dt} = \int_{\Omega_e} F(W_i) \cdot \nabla \phi_j d\Omega - \sum_{e=1}^4 \int_{\Gamma_e} \phi_j \hat{F}_{i,e} \cdot n_{i,e} d\Gamma, \quad i = 1, \dots, N_e.$$

- Local mass and rigidity matrices.
- Numerical flux \hat{F} .
- High order scheme in space and time with SSP Runge Kutta time integrators

¹[Cockburn, Shu, 1998],[Gottlieb, Ketcheson, Shu, 2009]

Outline

1 Context

- Global
- Transport of a polydisperse spray

2 Realizable high order methods

- Kinetic Finite Volume schemes
- Runge Kutta Discontinuous Galerkin methods

3 Slope limitation

- Principle
- Properties
- Projection method

4 Numerical results

Limitation and realizability

Theorem [Zhang, Shu, 2010, 2012]

G , convex set of realizable states.

Assuming:

- $W_i(T^n) \in G$ and \hat{F} , realizable.
- Realizability at quadrature nodes x_q : $W_i^q \in G$
- CFL condition: $\frac{\Delta t \lambda_i}{\Delta x} \leq \min_q \omega_q$.

then the DG solution at T^{n+1} is realizable.

Convex moments set \mathcal{G} :

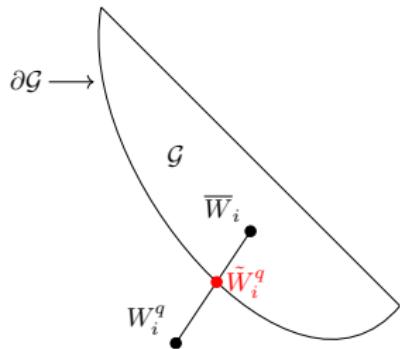
$$\tilde{W}_i^q = \theta_q W_i^q + (1 - \theta_q) \bar{W}_i$$

$$\tilde{W}_i = \theta_i (W_i - \bar{W}_i^{n+1}) + \bar{W}_i^{n+1}, \quad \theta_i = \min_q \theta_q$$

→ Properties: conservative, accuracy

Challenges

- High order moment models
- **Projection method**
- Stability near the boundary of the moments set



Projection method

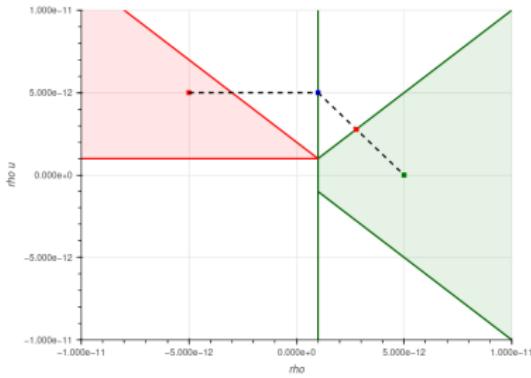
Step-by-step projection

- Realizability constraint:

$$\tilde{\rho}^1 = \theta^1 \rho + (1 - \theta^1) \bar{\rho}$$

- Maximum principle on the velocity:

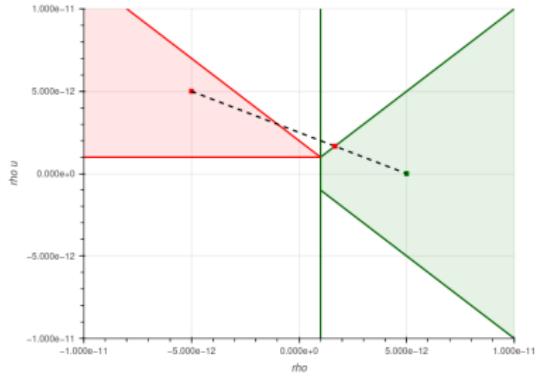
$$\left(\begin{array}{c} \tilde{\rho} \\ \tilde{\rho} u \end{array} \right) = \theta^2 \left(\begin{array}{c} \tilde{\rho}^1 \\ \rho u \end{array} \right) + (1 - \theta^2) \left(\begin{array}{c} \bar{\rho} \\ \bar{\rho} u \end{array} \right)$$



Straight projection

Realizability constraint and maximum principle on the velocity:

$$\left(\begin{array}{c} \tilde{\rho} \\ \tilde{\rho} u \end{array} \right) = \theta \left(\begin{array}{c} \rho \\ \rho u \end{array} \right) + (1 - \theta) \left(\begin{array}{c} \bar{\rho} \\ \bar{\rho} u \end{array} \right)$$



→ Do they preserve the order accuracy of the DG method?

Order accuracy

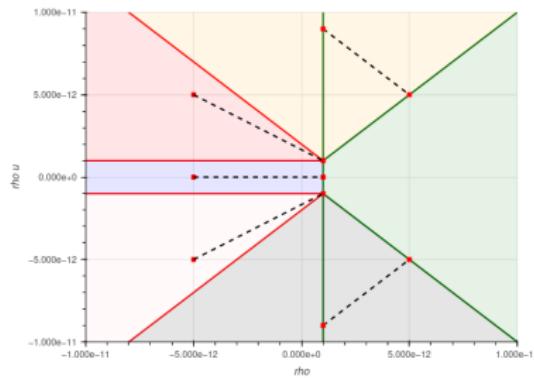
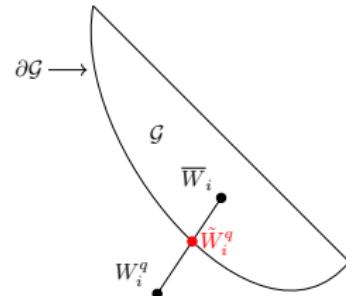
Conditionnal preservation of the order

$$\begin{aligned} \|\tilde{W}_i^q - W_{ex}\| &= (1 - \theta)\|\bar{W}_i - W_{ex}\| + \theta\|W_i^q - W_{ex}\| \\ &\leq (1 - \theta)\mathcal{O}(\Delta x) + \theta\mathcal{O}(\Delta x^{k+1}) \end{aligned}$$

- **Hypothesis:** $d(W_{ex}, \partial\mathcal{G}) \geq M$.
- $1 - \theta = \frac{\|\tilde{W}_i^q - W_i^q\|}{\|W_i^q - \bar{W}_i\|} \leq \mathcal{O}(\Delta x^{k+1})$

Unconditionnal preservation of the order

- $\mathcal{P}_{\min} W_i^q = \operatorname{argmin}_{V \in \mathcal{G}} \|W_i^q - V\|$
- Does not provide conservative projection method



Comparisons of projections

Admissible set:

$$G = \{\rho > \epsilon, \quad \rho u_{\min} \leq \rho u \leq \rho u_{\max}\}$$

- Orange region:

$$\mathcal{P}_{Straight} = \mathcal{P}_{Zhang} \text{ and } \mathcal{P}_{\min} = \mathcal{P}_{\rho u=\rho u_{\max}}^{\perp}$$

- Red region:

$$\mathcal{P}_{Straight} \neq \mathcal{P}_{Zhang} \text{ and } \mathcal{P}_{\min} = (\epsilon, \epsilon u_{\max})$$

- Blue region:

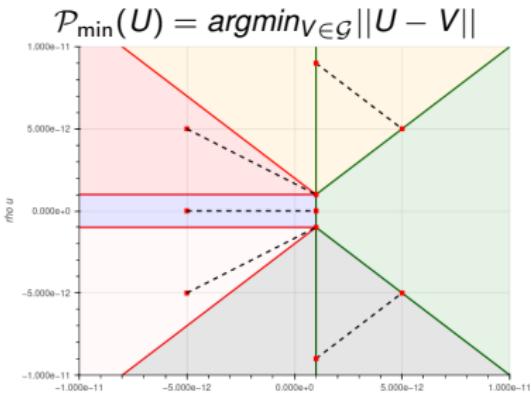
$$\mathcal{P}_{Straight} \neq \mathcal{P}_{Zhang} = \mathcal{P}_{\min} = \mathcal{P}_{\rho=\epsilon}^{\perp}$$

- Pink region:

$$\mathcal{P}_{Straight} \neq \mathcal{P}_{Zhang} \text{ and } \mathcal{P}_{\min} = (\epsilon, \epsilon u_{\min})$$

- Grey region:

$$\mathcal{P}_{Straight} = \mathcal{P}_{Zhang} \text{ and } \mathcal{P}_{\min} = \mathcal{P}_{\rho u=\rho u_{\min}}^{\perp}$$



→ Behavior at the vacuum limit for \mathcal{P}_{Zhang} and $\mathcal{P}_{Straight}$:

$$\left(\frac{\bar{\rho}}{\rho u} \right) \rightarrow \left(\frac{\epsilon}{\epsilon u} \right), u_{\min} \leq u \leq u_{\max}$$

Behavior at the vacuum limit

- Zhang and Shu projection method:

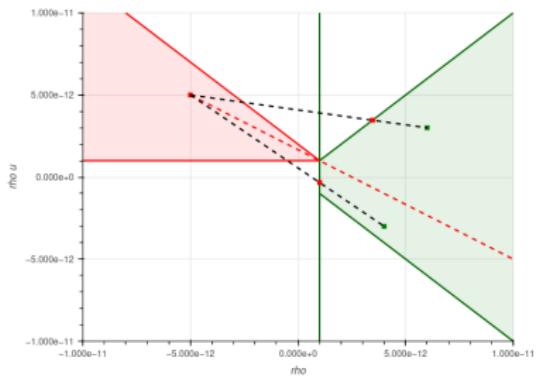
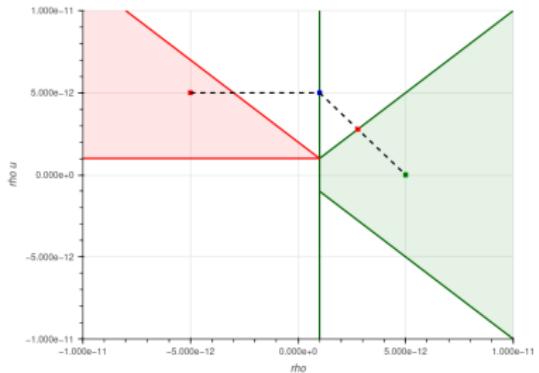
$$\left\{ \begin{array}{l} (i) \quad \rho \longrightarrow \epsilon \\ (ii) \quad (\epsilon, \rho u) \longrightarrow (\tilde{\rho}, \tilde{\rho} u) \\ \left(\frac{\tilde{\rho}}{\tilde{\rho} u} \right) = \theta_{\rho u} \left(\frac{\epsilon}{\rho u} \right) + (1 - \theta_{\rho u}) \left(\frac{\bar{\rho}}{\bar{\rho} u} \right) \end{array} \right.$$

- Straight projection:

$$\left\{ \begin{array}{l} (\rho, \rho u) \longrightarrow (\tilde{\rho}, \tilde{\rho} u) \\ \left(\frac{\tilde{\rho}}{\tilde{\rho} u} \right) = \theta \left(\frac{\rho}{\rho u} \right) + (1 - \theta) \left(\frac{\bar{\rho}}{\bar{\rho} u} \right), \\ \theta = \max(\theta_\rho, \theta_{\rho u}) \end{array} \right.$$

Choice of projection method

Straight projection preserves all the properties.



High order moment model

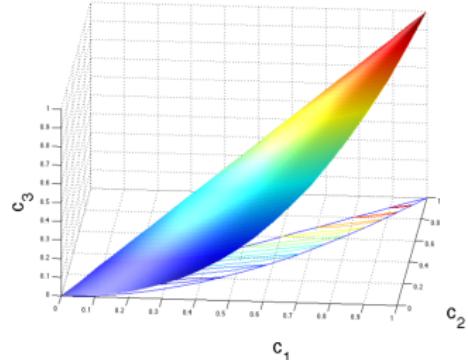
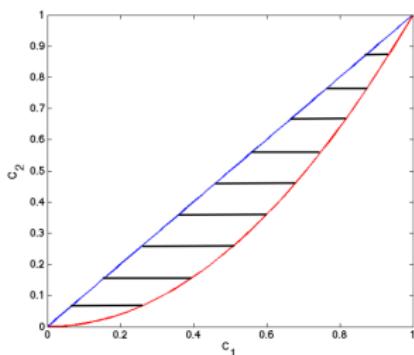
$$\partial_t W + \partial_x F(W) = 0, \quad W = (m_0, m_{1/2}, m_1, m_{3/2}, m_1 u) \in \mathbb{M}_3^{1/2}$$

Characterisation of moments set with Hankel determinants [Dette and Studden, 1997]

$$\vec{m}_{N/2} = (m_0, m_{1/2}, \dots, m_{N/2}) \in \mathbb{M}_N^{1/2} \Leftrightarrow \underline{H}_i \text{ and } \bar{H}_i \text{ are non negative for } i = 0, \dots, N.$$

First constraints: $m_0 > 0$ and for $c_{k/2} = \frac{m_{k/2}}{m_0}$:

$$c_{1/2} > 0, \quad c_{1/2}^2 < c_1 < c_{1/2}, \quad \frac{c_1^2}{c_{1/2}} < c_{3/2} < \frac{c_1^2}{c_{1/2}} + \frac{(c_1 - c_{1/2}^2)(c_{1/2} - c_1)}{c_{1/2}(1 - c_{1/2})}$$



Straight projection for moment models

For each quadrature point q :

- If $\underline{H}_i < 0$, or $\bar{H}_i < 0$:

$$(\tilde{m}_{i/2})_q = (\bar{m}_{i/2}) + \theta_q^i [(m_{i/2})_q - \bar{m}_{i/2}], \quad \theta_q^i \in [0, 1],$$

such that: $\underline{H}_i = 0$, $\bar{H}_i = 0$, $i = 0, \dots, 3$.

- If $(m_1 u)_q > (m_1)_q u_{\max}$:

$$(\tilde{m}_1 u)_q = (\bar{m}_1 u) + \theta_q^4 [(m_1 u)_q - (\bar{m}_1 u)], \quad \theta_q^4 \in [0, 1],$$

such that: $(\tilde{m}_1 u)_q = (m_1)_q u_{\max}$.

For each cell:

$$\begin{pmatrix} (\tilde{m}_0)_q \\ (\tilde{m}_{1/2})_q \\ (\tilde{m}_1)_q \\ (\tilde{m}_{3/2})_q \\ (\tilde{m}_1 u)_q \end{pmatrix} = \begin{pmatrix} \bar{m}_0 \\ \bar{m}_{1/2} \\ \bar{m}_1 \\ \bar{m}_{3/2} \\ (m_1 u) \end{pmatrix} + \theta \left[\begin{pmatrix} (\tilde{m}_0)_q \\ (\tilde{m}_{1/2})_q \\ (\tilde{m}_1)_q \\ (\tilde{m}_{3/2})_q \\ (\tilde{m}_1 u)_q \end{pmatrix} - \begin{pmatrix} \bar{m}_0 \\ \bar{m}_{1/2} \\ \bar{m}_1 \\ \bar{m}_{3/2} \\ (m_1 u) \end{pmatrix} \right], \quad \theta = \min_q (\theta_q^0, \theta_q^1, \theta_q^2, \theta_q^3, \theta_q^4)$$

Outline

1 Context

- Global
- Transport of a polydisperse spray

2 Realizable high order methods

- Kinetic Finite Volume schemes
- Runge Kutta Discontinuous Galerkin methods

3 Slope limitation

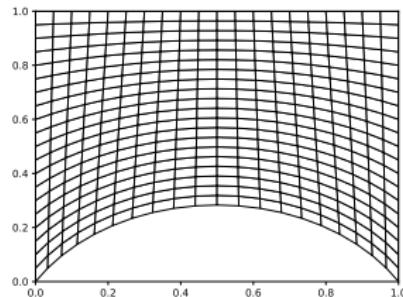
- Principle
- Properties
- Projection method

4 Numerical results

Josiepy, a PDE solver written in Python

$$\frac{\partial q}{\partial t} + \nabla \cdot F(q) + B(q) \cdot \nabla q - \nabla \cdot (K(q) \cdot \nabla q) + s(q) = 0$$

- Euler solver (including an exact RP solver for generic EOS)
- Baer-Nunziato solver
- Compressible Navier Stokes
- Heat Equation
- Baer Nunziato model enriched with geometrical variables.
- Ode solvers, arbitrary RK methods
- Composite BC
- Runge Kutta Discontinuous Galerkin schemes

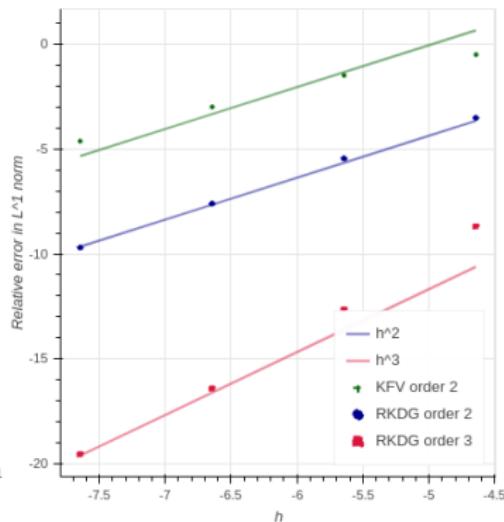
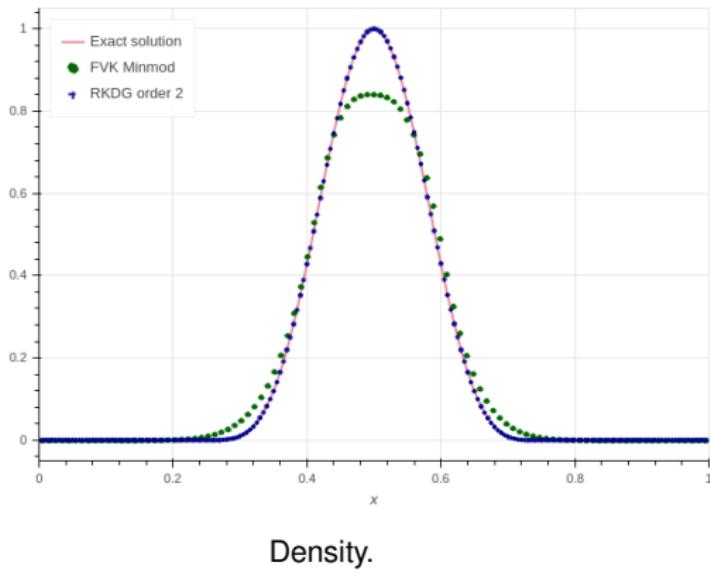


[https://gitlab.com/
rubendibattista/josiepy](https://gitlab.com/rubendibattista/josiepy)

Advection

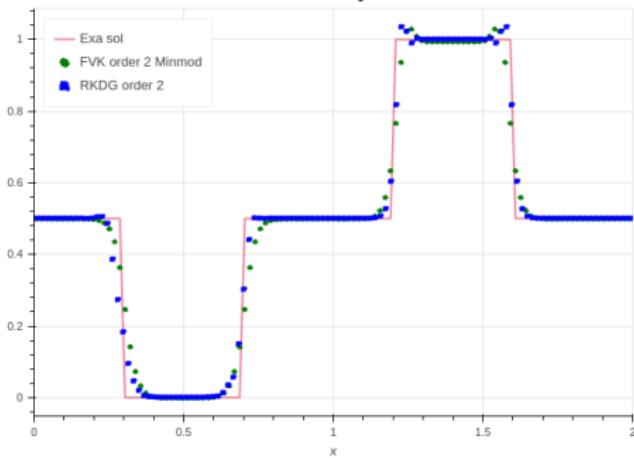
Gaussian initial condition:

$$u(x) = 1, \rho(x, 0) = \begin{cases} (\cos(\pi(2x - 1)))^4 & \text{if } 0.25 < x < 0.75, \\ 0 & \text{otherwise} \end{cases}$$

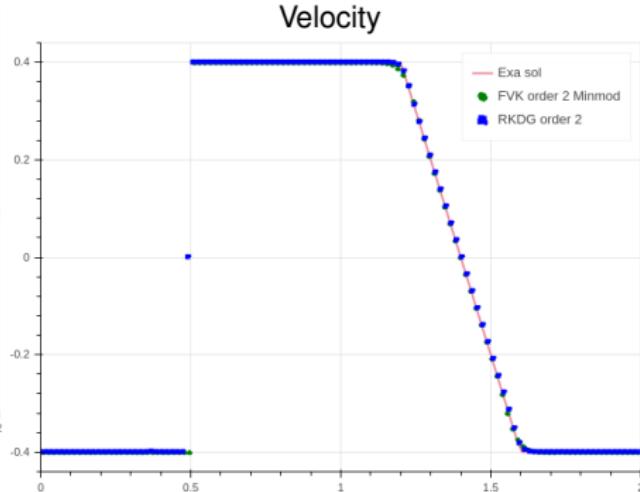


Vacuum test case

Density



Velocity



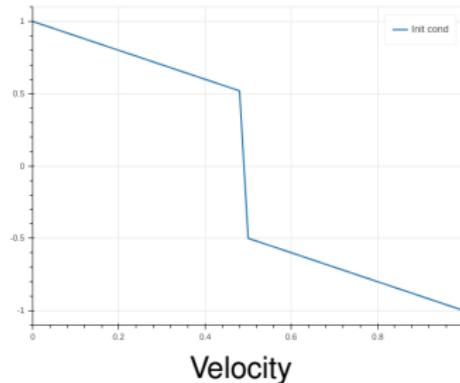
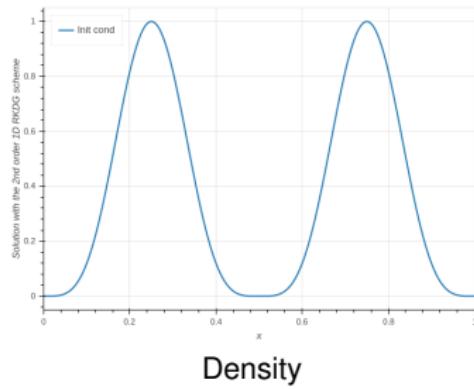
Mesh size	Order 2	
	Zhang & Shu	Straight
$N = 25$	10^{-6}	10^{-8}
$N = 50$	10^{-6}	10^{-12}
$N = 100$	10^{-9}	10^{-12}
$N = 200$	10^{-12}	10^{-12}

→ Robustness for accumulation zones and vacuum states.

PGD system - δ -shock

Initial condition generating δ -shocks:

$$\rho(x, 0) = (\sin(2\pi x))^4, u(x, 0) = \begin{cases} -x & \text{if } x > 0.5, \\ -x + 1 & \text{otherwise} \end{cases}$$

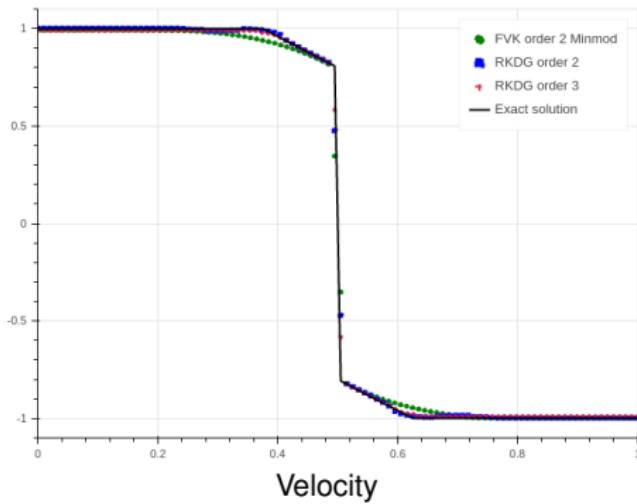
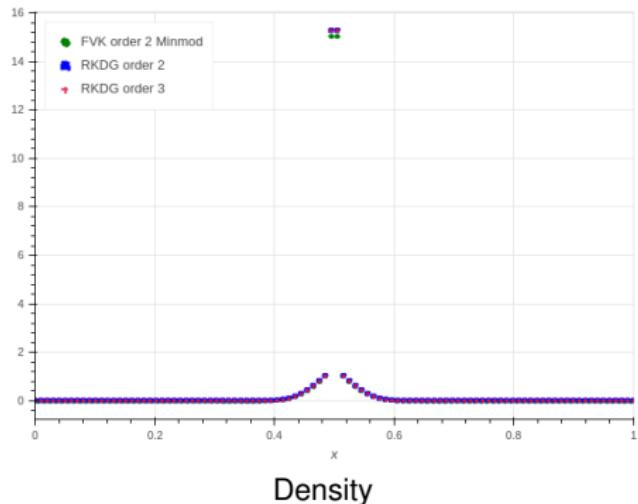


Realizability domain:

$$G := \left\{ \begin{pmatrix} \rho_i \\ \rho_i u_i \end{pmatrix}, \rho_i > 0, \quad m_i \leq u_i \leq M_i \right\}, \quad m_i = \min(u_{i-1}, u_i, u_{i+1}), \quad M_i = \max(u_{i-1}, u_i, u_{i+1})$$

δ -shock

Initial condition: $\rho(x, 0) = (\sin(2\pi x))^4$, $u(x, 0) = \begin{cases} -x & \text{if } x > 0.5, \\ -x + 1 & \text{, otherwise} \end{cases}$



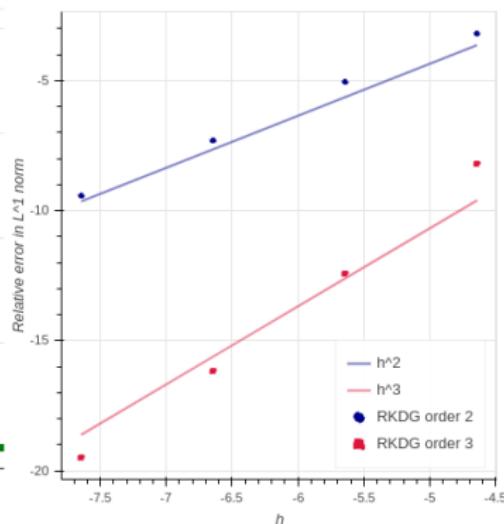
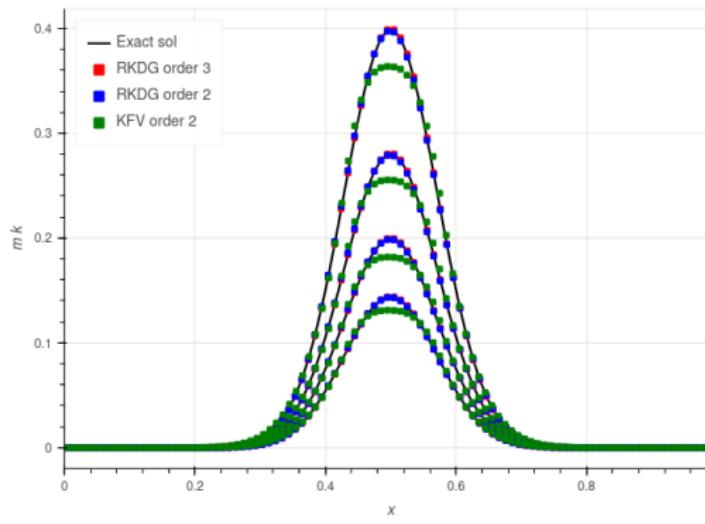
→ Robustness for δ -shock singularities and numerical diffusion of the velocity profile.

Advection

Initial moments:

$$m_{k/2}(x, 0) = \frac{2}{k+2} \left(S_{\max}^{(k+2)/2} - S_{\min}^{(k+2)/2} \right) \exp \left(-\frac{(x - x_c)^2}{\sigma_x^2} \right), \quad u(x) = -1,$$

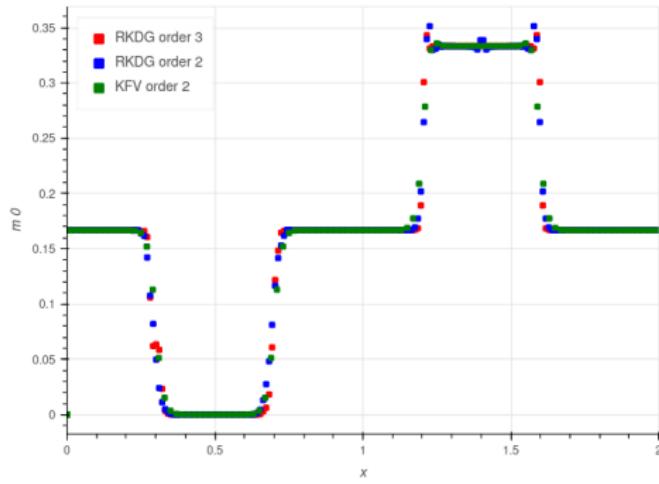
$$(S_{\min}, S_{\max}) = (0.3, 0.7), \quad x_c = 0.5, \quad \sigma_x = 0.1.$$



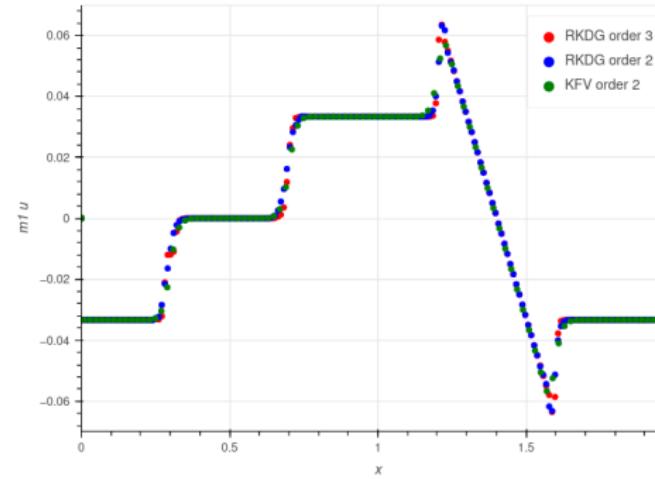
Vacuum test case

Initial condition:

$$m_k(x, 0) = (2 + k)^{-1} - (3 + k)^{-1}, u(x, 0) = \begin{cases} -0.4 & \text{if } 0.5 < x \text{ or } x > 1.8, \\ 0.4 & \text{if } 0.5 < x < 1, \\ 1.4 - x & \text{if } 1 < x < 1.8, \end{cases}$$



First moment m_0

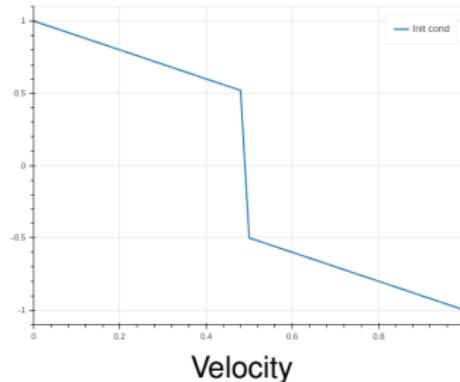
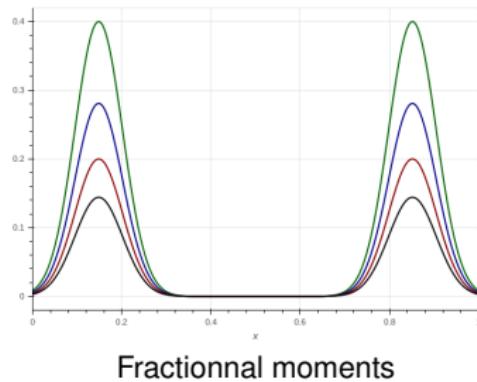


$m_1 u$

→ Robustness for accumulation zones and vacuum states.

δ -shock test case

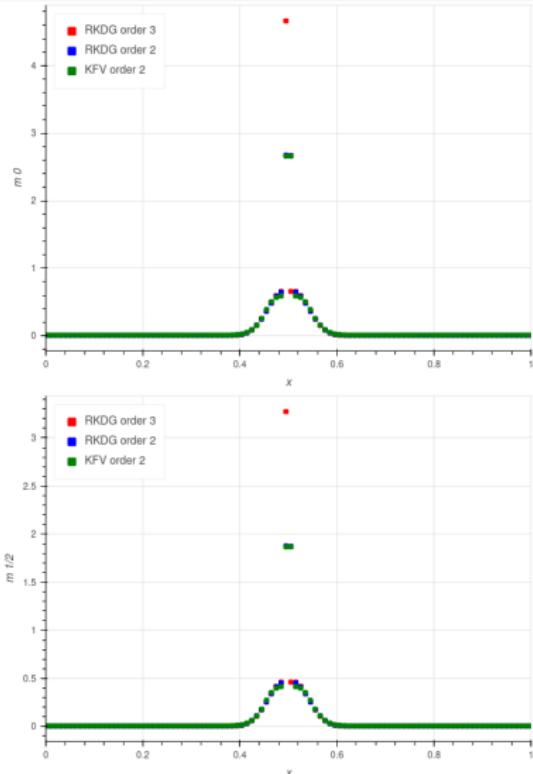
Initial condition:



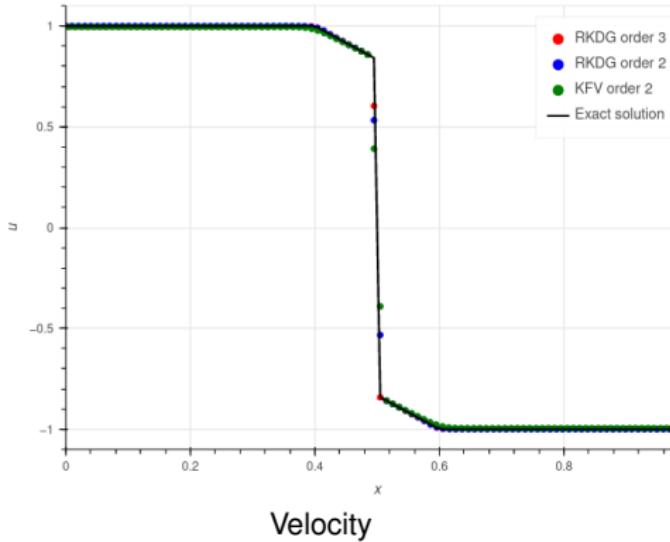
Realizability domain:

$$G := \left\{ \begin{pmatrix} (m_0)_i \\ (m_{1/2})_i \\ (m_1)_i \\ (m_{3/2})_i \\ (m_1)_i u_i \end{pmatrix}, \underline{H}_i(m_0, \dots, m_i) \geq 0, \bar{H}_i(m_0, \dots, m_i) \geq 0, \min_{C_i, C_{i \pm 1}} u \leq u_i \leq \max_{C_i, C_{i \pm 1}} u \right\}$$

δ -shock



First fractionnal moments: m_0 , $m_{1/2}$.

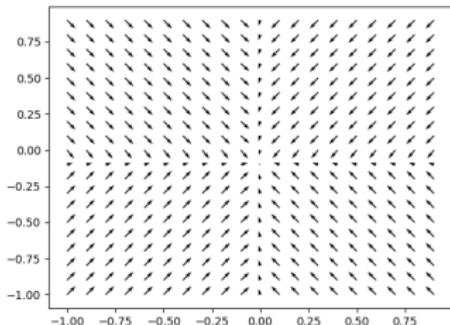
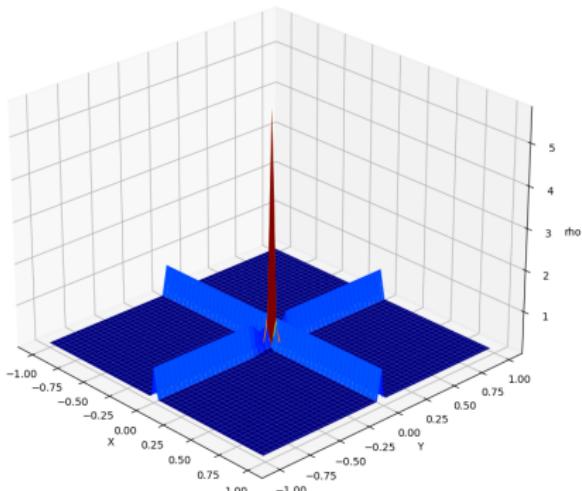


- Robustness for δ -shock singularities
- Stability near the boundary of moments set
- Numerical diffusion of the velocity profile

2D δ -shock test case

Initial condition:

$$m_k(x, y, 0) = (2+k)^{-1} - (3+k)^{-1}, \quad (u, v)(x, y, 0) = \begin{cases} (-0.25, -0.25) & x > 0, y > 0, \\ (0.25, -0.25) & x < 0, y > 0, \\ (0.25, 0.25) & x < 0, y < 0, \\ (-0.25, 0.25) & x > 0, y < 0 \end{cases}$$

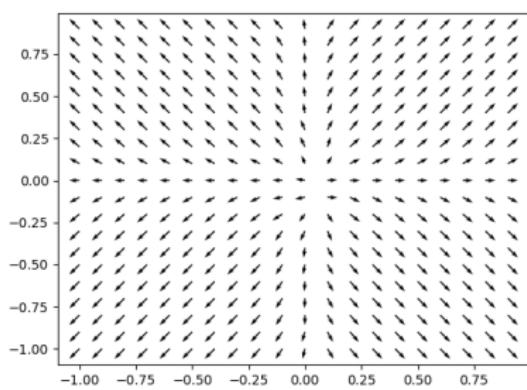
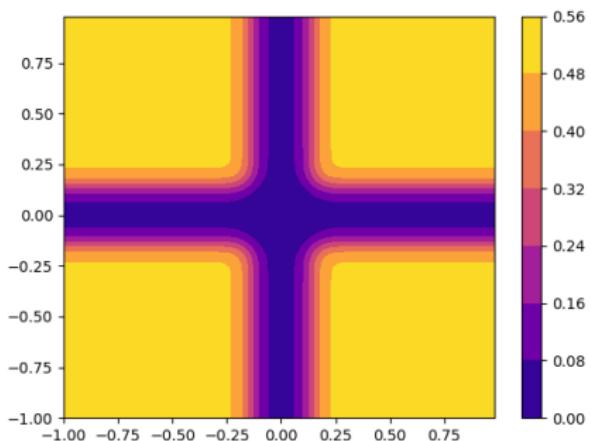


Fractionnal moment $m_{1/2}$ (left) and velocity field (right) at $t = 0.5$.

2D Vacuum test case

Initial condition:

$$m_k(x, y, 0) = (2+k)^{-1} - (3+k)^{-1}, \quad (u, v)(x, y, 0) = \begin{cases} (0.4, 0.4) & x > 0, y > 0, \\ (-0.4, 0.4) & x < 0, y > 0, \\ (-0.4, -0.4) & x < 0, y < 0, \\ (0.4, -0.4) & x > 0, y < 0 \end{cases}$$



Fractionnal moment $m_{1/2}$ (left) and velocity field (right) at $t = 0.4$.

Summary

- RKDG and the KFV are robust and accurate for the capture of **singularities in moments models**.
- **Straight projection** method: conservative, order accuracy and stability near the boundary of moments set.
- Slope limiters for KFV scheme **smear out discontinuities**.
- **Realizable and maximum principle** satisfying RKDG schemes [Ait Ameur et al, in preparation]

Outlook

- Extension to more complex moment models for the disperse phase:
 - Accounting for the **oscillations of the droplets** in the spray: $\Xi = (S, \dots)$
 - Treat additionnal phenomena: **evaporation**, drag force.
- **Link with separated phase models** enriched by subscale flow modelling, [Loison et al, in preparation]
- Numerical method for Baer Nunziato type models: **Lagrange projection splitting method** [Ait Ameur et al, in preparation]
- **HPC**: adaptive multiresolution SAMURAI library [Gouarin et al, 2021]

Thank you for your attention.